Electricity and New Energy

Conventional DC Machines and Universal Motor

Courseware Sample

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Safety and Common Symbols

The following safety and common symbols may be used in this manual and on the equipment:

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<th>Symbol</th>
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<tr>
<td><img src="image" alt="DANGER" /></td>
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<td>Off (supply)</td>
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<tr>
<td><img src="image6" alt="Symbol" /></td>
<td>Equipment protected throughout by double insulation or reinforced insulation</td>
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<td><img src="image7" alt="Symbol" /></td>
<td>In position of a bi-stable push control</td>
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<tr>
<td><img src="image8" alt="Symbol" /></td>
<td>Out position of a bi-stable push control</td>
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The production of energy using renewable natural resources such as wind, sunlight, rain, tides, geothermal heat, etc., has gained much importance in recent years as it is an effective means of reducing greenhouse gas (GHG) emissions. The need for innovative technologies to make the grid smarter has recently emerged as a major trend, as the increase in electrical power demand observed worldwide makes it harder for the actual grid in many countries to keep up with demand. Furthermore, electric vehicles (from bicycles to cars) are developed and marketed with more and more success in many countries all over the world.

To answer the increasingly diversified needs for training in the wide field of electrical energy, the Electric Power Technology Training Program was developed as a modular study program for technical institutes, colleges, and universities. The program is shown below as a flow chart, with each box in the flow chart representing a course.
Preface

The program starts with a variety of courses providing in-depth coverage of basic topics related to the field of electrical energy such as ac and dc power circuits, power transformers, rotating machines, ac power transmission lines, and power electronics. The program then builds on the knowledge gained by the student through these basic courses to provide training in more advanced subjects such as home energy production from renewable resources (wind and sunlight), large-scale electricity production from hydropower, large-scale electricity production from wind power (doubly-fed induction generator [DFIG], synchronous generator, and asynchronous generator technologies), smart-grid technologies (SVC, STATCOM, HVDC transmission, etc.), storage of electrical energy in batteries, and drive systems for small electric vehicles and cars.

Do you have suggestions or criticism regarding this manual?

If so, send us an e-mail at did@de.festo.com.

The authors and Festo Didactic look forward to your comments.
About This Manual

This course, *Conventional DC Machines and Universal Motor*, first describes the operation of the prime mover and brake used throughout the hands-on exercises. The student learns how to determine the polarity of the speed, torque, and mechanical power measured for a machine operating as either a motor or a generator. The course then introduces the student to the operation and characteristics of the following rotating machines: separately-excited, shunt, series, and compound dc motors, separately-excited, shunt, and compound dc generators, and universal motor. These machines, although still in use in numerous applications today, are less common in modern battery-powered applications (e.g., electric bicycles, mobility scooters, etc.) where power efficiency is at a premium.

Safety considerations

Safety symbols that may be used in this manual and on the equipment are listed in the Safety Symbols table at the beginning of the manual.

Safety procedures related to the tasks that you will be asked to perform are indicated in each exercise.

Make sure that you are wearing appropriate protective equipment when performing the tasks. You should never perform a task if you have any reason to think that a manipulation could be dangerous for you or your teammates.

Prerequisite

As a prerequisite to this course, you should have read the manuals titled *DC Power Circuits*, part number 86350 and *Single-Phase AC power Circuits*, part number 86358.

Systems of units

Units are expressed using the International System of Units (SI) followed by the units expressed in the U.S. customary system of units (between parentheses).
To the Instructor

You will find in this Instructor Guide all the elements included in the Student Manual together with the answers to all questions, results of measurements, graphs, explanations, suggestions, and, in some cases, instructions to help you guide the students through their learning process. All the information that applies to you is placed between markers and appears in red.

Accuracy of measurements

The numerical results of the hands-on exercises may differ from one student to another. For this reason, the results and answers given in this manual should be considered as a guide. Students who correctly performed the exercises should expect to demonstrate the principles involved and make observations and measurements similar to those given as answers.

Equipment installation

In order for students to be able to perform the exercises in the Student Manual, the Electric Power Technology Training Equipment must have been properly installed, according to the instructions given in the user guide Electric Power Technology Training Equipment, part number 38486-E.
Sample Exercise

Extracted from
the Student Manual
and the Instructor Guide
DC Motors and Generators

UNIT OBJECTIVE
When you have completed this unit, you will be able to use the DC Motor/Generator to demonstrate and explain the operation of dc motors and generators.

DISCUSSION OUTLINE
The Discussion of Fundamentals covers the following points:

- Operating principle of dc motors
- Operating principle of dc generators

DISCUSSION OF FUNDAMENTALS

Operating principle of dc motors

As stated in Unit 1, motors turn because of the interaction between two magnetic fields. This unit will discuss how these magnetic fields are produced in dc motors, and how magnetic fields induce voltage in dc generators.

The basic principle of a dc motor is the creation of a rotating magnet inside the mobile part of the motor, the rotor. This is accomplished by a device called the commutator, which is found on all dc machines. The commutator produces the alternating currents necessary for the creation of the rotating magnet from dc power provided by an external source. Figure 2-1 shows a typical dc motor rotor with its main parts. This figure shows that the electrical contact between the segments of the commutator and the external dc power source $E_S$ is made through brushes. Note that the rotor of a dc motor is also referred to as the armature.

![Diagram of a dc motor rotor](image)

Figure 2-1. The main parts of a dc motor rotor (armature).
Figure 2-2 and Figure 2-3 show what happens to the magnetic field in the armature wire loops when the rotor of the dc motor in Figure 2-1 rotates. In Figure 2-2a, the brushes make contact with commutator segments A and B. Therefore, current flows from the dc power source to wire loop A-B via the brushes. No current flows in wire loop C-D. This creates an electromagnet A-B with north and south poles, as shown in Figure 2-2a. When the rotor is rotated clockwise a little as in Figure 2-2b, current still flows in wire loop A-B, and the north and south poles of the electromagnet are rotated clockwise.

As the rotor continues to rotate clockwise, the commutator slots pass by the brushes and a commutation occurs, i.e., the brushes stop making contact with commutator segments A and B and make contact with commutator segments C.
and D instead, as shown in Figure 2-2c. Consequently, current stops flowing in wire loop A-B and starts to flow in wire loop C-D. This creates an electromagnet C-D with north and south poles, as shown in Figure 2-2c.

A comparison of Figure 2-2b and Figure 2-2c shows that, at commutation, the north and south poles of the electromagnet are rotated 90° counterclockwise. As the rotor continues to rotate clockwise, the same phenomenon repeats every 90° rotation (i.e., at every commutation), as shown in Figure 2-3.

Figure 2-3. Magnetic field produced at the armature when the rotor rotates clockwise (part II).
In summary, as the rotor rotates, the north and south poles of the electromagnet go back and forth (oscillate) over a 90° angle, as Figure 2-4 shows. In other words, the north and south poles can be considered as stationary, i.e., they do not rotate as the rotor rotates. This is equivalent to having an electromagnet in the rotor that rotates at the same speed as the rotor, but in the opposite direction.

The higher the number of segments on the commutator, the lower the angle of rotation between each commutation, and thus, the lower the angle over which the north and south poles of the electromagnet oscillate. For example, if the commutator shown in Figure 2-1, Figure 2-2, and Figure 2-3 were having 32 segments instead of 4, the north and south poles would oscillate over an angle of only 11.25° instead of 90°.

![Figure 2-4. The north and south poles of the electromagnet at the armature oscillate around a fixed position.](image)

When this rotor is placed next to a fixed permanent magnet stator as shown in Figure 2-5, the magnetic poles of opposite polarities attract each other (in order to align), while the magnetic poles of the same polarity repel each other, and the rotor starts to turn. After the rotor has turned by a certain angle, a commutation occurs and the north and south poles of the electromagnet go back to their initial location. Once again, the magnetic poles of opposite polarity attract each other (in order to align), while the magnetic poles of the same polarity repel each other, and the rotor starts to turn, and the rotor continues to rotate in the same direction. However, another commutation occurs a little after and the north and south poles of the electromagnet go back to their initial location once again. This cycle repeats over and over. The force that results from the interaction of the two magnetic fields always acts in the same direction, and the rotor turns continually. Thus, a rotating machine converting electrical energy into mechanical energy, i.e. an electric motor, is achieved. The direction of rotation depends on the polarity of the voltage applied to the brushes of the rotor.
Operating principle of dc generators

Previously, you saw that the variation of magnetic flux in a loop of wire causes a voltage to be induced across the ends of the loop. When a wire loop is placed between two magnets and rotated as shown in Figure 2-6, the magnetic flux $\phi$ that passes through the loop varies and a voltage, $E_1$, is induced across the loop terminals. Voltage $E_1$ is collected by the two commutator segments and delivered to stationary brushes ($B^+$ and $B^-$) connected to the generator terminals.

- As the loop passes from position 0 to position 4, the magnetic flux $\phi$ in the loop passes from a negative maximum (maximum flux passing from the A side to the B side of the loop) to a positive maximum (maximum flux passing from the B side to the A side of the loop). During this 180° interval of rotation, the voltage $E_1$ induced across the loop has a positive polarity because the rate of change $\frac{\Delta \phi}{\Delta t}$ of the magnetic flux has a positive value.

- When the loop reaches position 4, the connections of the two commutator segments to brushes $B^-$ and $B^+$ are reversed. Consequently, this reverses the connections between the wire loop terminals and the generator terminals.

- As the loop passes from position 4 to position 0, the magnetic flux $\phi$ in the loop passes from a positive maximum (maximum flux passing from the B side to the A side of the loop) to a negative maximum (maximum flux passing from the A side to the B side of the loop). During this 180° interval of rotation, the voltage $E_1$ induced across the loop has a negative polarity because the rate of change $\frac{\Delta \phi}{\Delta t}$ of the magnetic flux has a negative value.

- When the loop reaches position 0, the connections of the two commutator segments to brushes $B^-$ and $B^+$ are reversed again, thereby
reversing the connections between the wire loop terminals and the generator terminals.

This cycle repeats as long as the rotor continues to rotate, so that the polarity of the voltage $E_1$ generated across the rotor wire loop continually alternates: it is positive for half a turn, then negative for the next half turn, then positive for the next half turn, and so on. Because of this, the voltage $E_1$ generated across the rotor wire loop is referred to as an alternating-current (ac) voltage. Because the commutator reverses the connections between the wire loop terminals and the generator terminals at wire loop positions 0 and 4, the voltage $E_2$ at the generator terminals always has the same polarity (positive), as is shown in Figure 2-6. The voltage $E_2$ at the generator terminals is thus a pulsating positive direct current (dc) voltage (two pulses per rotation).

The faster the speed of rotation of the rotor, the higher the rate of change of the magnetic flux $\phi$ passing through the wire loop, and therefore, the higher the voltage $E_2$ at the generator terminals. Also, the stronger the magnetic field of the permanent magnet, the higher the intensity of the magnetic flux, and therefore, the higher the voltage $E_2$ at the generator terminals.
In Figure 2-6, the A side of the wire loop designates the plane of the loop viewed from the north (N) pole, while the B side of the wire loop designates the plane of the loop viewed from the south (S) pole.

Figure 2-6. A wire loop rotating in a magnetic field results in an induced voltage (clockwise rotation).
When the direction of rotation of the wire loop is reversed, the polarity of the dc voltage $E_2$ at the generator terminals also reverses, as Figure 2-7 shows. The voltage $E_2$ at the generator terminals is thus a pulsating negative dc voltage (two pulses per rotation).

Figure 2-7. When the direction of rotation of the wire loop is reversed, the polarity of the dc voltage at the generator terminals also reverses.
The Separately-Excited DC Motor

**EXERCISE OBJECTIVE**
When you have completed this exercise, you will be able to demonstrate the main operating characteristics of a separately-excited dc motor using the DC Motor/Generator.

**DISCUSSION OUTLINE**
The Discussion of this exercise covers the following points:

- Simplified equivalent circuit of a dc motor
- Relationship between the motor rotation speed and the armature voltage when the armature current is constant
- Relationship between the motor torque and the armature current
- Relationship between the motor rotation speed and the armature voltage when the armature current varies

**DISCUSSION**

**Simplified equivalent circuit of a dc motor**

Previously, you saw that a dc motor is made up of a fixed magnet (stator) and a rotating magnet (rotor). Many dc motors use an electromagnet at the stator, as Figure 2-8 shows.

![Simplified dc motor using an electromagnet as stator](image)

Figure 2-8. Simplified dc motor using an electromagnet as stator.

When power for the stator electromagnet is supplied by a separate dc source, of either fixed or variable voltage, the motor is known as a **separately-excited dc motor**. Sometimes the term independent-field dc motor is also used. The
ex. 2-1 – the separately-excited dc motor • discussion

current flowing in the stator electromagnet is often called field current because it is used to create a fixed magnetic field.

The electrical and mechanical behavior of the dc motor can be understood by examining its simplified equivalent electric circuit shown in Figure 2-9.

![Simplified equivalent circuit of a dc motor.](image)

In the circuit, $E_A$ is the voltage applied to the motor brushes, $I_A$ is the current flowing in the armature through the brushes, and $R_A$ is the resistance between the brushes. Note that $E_A$, $I_A$, and $R_A$ are usually referred to as the armature voltage, current, and resistance, respectively. $E_{RA}$ is the voltage drop across the armature resistor. When the motor turns, an induced voltage $E_{CEMF}$ proportional to the speed of the motor is produced. This induced voltage is represented by a dc source in the simplified equivalent circuit of Figure 2-9. The motor also develops a torque $T$ proportional to the armature current $I_A$ flowing in the motor. The motor behavior is based on the two equations given below. Equation (2-1) relates motor speed $n$ and the induced voltage $E_{CEMF}$. Equation (2-2) relates the motor torque $T$ and the armature current $I_A$.

$$n = K_1 \cdot E_{CEMF} \quad (2-1)$$

where $n$ is the motor rotation speed, expressed in revolutions per minute (r/min).

$K_1$ is a constant expressed in $\frac{r/min}{V}$.

$E_{CEMF}$ is the voltage induced across the armature, expressed in volts (V).

$$T = K_2 \cdot I_A \quad (2-2)$$

where $T$ is the motor torque, expressed in newton-meters (N·m) or in pound-force inches (lbf·in).

$K_2$ is a constant expressed in $\frac{N\cdot m}{A}$ or $\frac{lbf\cdot in}{A}$.

$I_A$ is the armature current, expressed in amperes (A).
Relationship between the motor rotation speed and the armature voltage when the armature current is constant

When a voltage $E_A$ is applied to the armature of a dc motor with no mechanical load, the armature current $I_A$ flowing in the equivalent circuit of Figure 2-9 is constant and has a very low value. As a result, the voltage drop $E_{RA}$ across the armature resistor is so low that it can be neglected, and $E_{CEMF}$ can be considered to be equal to the armature voltage $E_A$. Therefore, the relationship between the motor rotation speed $n$ and the armature voltage $E_A$ is a straight line because $E_{CEMF}$ is proportional to the motor rotation speed $n$. This linear relationship is shown in Figure 2-10. The slope of the straight line equals constant $K_1$.

Figure 2-10. Linear relationship between the motor rotation speed and the armature voltage.

Since the relationship between voltage $E_A$ and the rotation speed $n$ is linear, a dc motor can be considered to be a linear voltage-to-speed converter, as shown in Figure 2-11.

Figure 2-11. DC motor as a voltage-to-speed converter.
Relationship between the motor torque and the armature current

The same type of relationship exists between the motor torque $T$ and the armature current $I_A$, so that a dc motor can also be considered as a linear current-to-torque converter. Figure 2-12 illustrates the linear relationship between the motor torque $T$ and the armature current $I_A$. Constant $K_2$ is the slope of the line relating the two. The linear current-to-torque converter is shown in Figure 2-13.

![Figure 2-12. Linear relationship between the motor torque and the armature current.](image1)

![Figure 2-13. DC motor as a current-to-torque converter.](image2)

Relationship between the motor rotation speed and the armature voltage when the armature current varies

When the armature current $I_A$ increases, the voltage drop $E_{RA} (R_A \cdot I_A)$ across the armature resistor also increases and can no longer be neglected. As a result, the armature voltage $E_A$ can no longer be considered equal to $E_{CEMF}$, but rather the sum of $E_{CEMF}$ and $E_{RA}$, as Equation (2-3) shows:

$$E_A = E_{CEMF} + E_{RA}$$ (2-3)
Therefore, when a fixed armature voltage $E_A$ is applied to a dc motor, the voltage drop $E_{RA}$ across the armature resistor increases as the armature current $I_A$ increases, and thereby, causes $E_{CEMF}$ to decrease. This also causes the motor rotation speed $n$ to decrease because it is proportional to $E_{CEMF}$. This is shown in Figure 2-14, which is a graph of the motor rotation speed $n$ versus the armature current $I_A$ for a fixed armature voltage $E_A$.

![Figure 2-14. The motor rotation speed drops as the armature current increases (fixed armature voltage $E_A$).](image)

Figure 2-15. Example of a separately-excited dc motor used in a racing kart.
The Procedure is divided into the following sections:

- Set up and connections
- Determining the armature resistance
- Motor speed versus armature voltage
- Motor torque versus armature current
- Speed decrease versus armature current
- Additional experiments (optional)
  
  Motor speed-versus-armature voltage and motor torque-versus-armature current characteristics for reversed armature connections.

### PROCEDURE

**WARNING**

High voltages are present in this laboratory exercise. Do not make or modify any banana jack connections with the power on unless otherwise specified.

**Set up and connections**

*In this section, you will mechanically couple the DC Motor/Generator to the Four-Quadrant Dynamometer/Power Supply and set up the equipment.*

1. Refer to the Equipment Utilization Chart in Appendix A to obtain the list of equipment required to perform the exercise. Install the equipment in the Workstation.

  Before performing the exercise, ensure that the brushes of the DC Motor/Generator are adjusted to the neutral point. To do so, connect a variable-voltage ac power source (terminals 4 and N of the Power Supply) to the armature of the DC Motor/Generator (terminals 1 and 2) through current input $I_1$ of the Data Acquisition and Control Interface (DACI). Connect the shunt winding of the DC Motor/Generator (terminals 5 and 6) to voltage input $E_1$ of the DACI. In LVDAC-EMS, open the Metering window. Set two meters to measure the rms values (ac) of the armature voltage $E_A$ and armature current $I_A$ at inputs $E_1$ and $I_1$ of the DACI, respectively. Turn the Power Supply on and adjust its voltage control knob so that an ac current (indicated by meter $I_1$ in the Metering window) equal to half the nominal armature current flows in the armature of the DC Motor/Generator. Adjust the brush adjustment lever on the DC Motor/Generator so that the voltage across the shunt winding (indicated by meter $E_1$ in the Metering window) is minimal. Turn the Power Supply off, close LVDAC-EMS, and disconnect all leads and cable.

Mechanically couple the DC Motor/Generator to the Four-Quadrant Dynamometer/Power Supply using a timing belt.

**WARNING**

Before coupling rotating machines, make absolutely sure that power is turned off to prevent any machine from starting inadvertently.
2. Make sure that the main power switch of the Four-Quadrant Dynamometer/Power Supply is set to the O (off) position, then connect its Power Input to an ac power wall outlet.

3. On the Power Supply, make sure that the main power switch and the 24 V ac power switch are set to the O (off) position, and that the voltage control knob is set to 0% (turned fully counterclockwise). Connect the Power Supply to a three-phase ac power outlet.

4. Connect the Power Input of the Data Acquisition and Control Interface (DACI) to the 24 V ac power source of the Power Supply.

   Turn the 24 V ac power source of the Power Supply on.

5. Connect the USB port of the Data Acquisition and Control Interface to a USB port of the host computer.

   Connect the USB port of the Four-Quadrant Dynamometer/Power Supply to a USB port of the host computer.

6. Connect the equipment as shown in Figure 2-16. Use the variable dc voltage output of the Power Supply to implement the variable-voltage dc power source $E_c$. Use the fixed dc voltage output of the Power Supply to implement the fixed-voltage dc power source. $E_1$, $I_1$ and $I_2$ are voltage and current inputs of the Data Acquisition and Control Interface (DACI). Leave the circuit open at points A and B shown in the figure.

7. On the Four-Quadrant Dynamometer/Power Supply, set the Operating Mode switch to Dynamometer. This setting allows the Four-Quadrant Dynamometer/Power Supply to operate as a prime mover, a brake, or both, depending on the selected function.

   Turn the Four-Quadrant Dynamometer/Power Supply on by setting the main power switch to the I (on) position.
8. Turn the host computer on, then start the LVDAC-EMS software.

In the LVDAC-EMS Start-Up window, make sure that the Data Acquisition and Control Interface and the Four-Quadrant Dynamometer/Power Supply are detected. Make sure that the Computer-Based Instrumentation function is available for the Data Acquisition and Control Interface module. Select the network voltage and frequency that correspond to the voltage and frequency of the local ac power network, then click the OK button to close the LVDAC-EMS Start-Up window.
9. In LVDAC-EMS, open the Four-Quadrant Dynamometer/Power Supply window, then make the following settings:

- Set the **Function** parameter to **Two-Quadrant, Constant-Torque Brake**. This setting makes the Four-Quadrant Dynamometer/Power Supply operate as a two-quadrant brake with a torque setting corresponding to the **Torque** parameter.

- Set the **Pulley Ratio** parameter to 24:24. The first and second numbers in this parameter specify the number of teeth on the pulley of the Four-Quadrant Dynamometer/Power Supply and the number of teeth on the pulley of the machine under test (i.e., the **DC Motor/Generator**), respectively.

- Make sure that the **Torque Control** parameter is set to **Knob**. This allows the torque of the two-quadrant brake to be controlled manually.

- Set the **Torque** parameter to the maximum value (3.0 N·m or 26.5 lbf·in). This sets the torque command of the **Two-Quadrant, Constant-Torque Brake** to 3.0 N·m (26.5 lbf·in).

  The torque command can also be set by using the **Torque** control knob in the Four-Quadrant Dynamometer/Power Supply window.

- Start the **Two-Quadrant, Constant-Torque Brake** by setting the **Status** parameter to **Started** or by clicking the **Start/Stop** button.

10. In LVDAC-EMS, open the **Metering** window. Set two meters to measure the dc motor armature voltage $E_A$ ($E1$) and armature current $I_A$ ($I1$). Set a meter to measure the dc motor armature resistance $R_A$ ($RDC (E1, I1)$). Finally, set a meter to measure the dc motor field current $I_F$ ($I2$).

Click the **Continuous Refresh** button to enable continuous refresh of the values indicated by the various meters in the **Metering** application.

**Determining the armature resistance**

*In this section, you will measure the armature resistance $R_A$ of the DC Motor/Generator. It is not possible to measure the armature resistance $R_A$ of the DC Motor/Generator with a conventional ohmmeter because the non-linear characteristic of the motor brushes causes incorrect results when the armature current $I_A$ is too low. The general method used to measure $R_A$ consists in connecting a dc power source to the motor armature and measuring the voltage required to make nominal current flow in the armature windings. No power source is connected to the motor stator to ensure that the motor does not rotate, and that $E_{CEMF}$ equals zero. The ratio of the armature voltage $E_A$ to the armature current $I_A$ yields the armature resistance $R_A$ directly.*

The motor will not start rotating because it is mechanically loaded.
11. Turn the **Power Supply** on by setting the main power switch to the I (on) position. Set the voltage control knob of the **Power Supply** so that the armature current $I_A$ (indicated by meter $I1$ in the **Metering** window) flowing in the **DC Motor/Generator** is equal to the rated armature current.

   The rating of any of the supplied machines is indicated in the lower section of the module front panel.

Record the value of the armature resistance $R_A$ [indicated by meter $RDC (E1, I1)$ in the **Metering** window].

Armature resistance $R_A = \phantom{0}7.6 \phantom{0} \Omega$

12. On the **Power Supply**, set the voltage control knob to 0%, then set the main power switch to the O (off) position. (Leave the 24 V ac power source of the **Power Supply** turned on.)

   Interconnect points A and B in the circuit of Figure 2-16.

**Motor speed versus armature voltage**

In this section, you will measure data and plot a graph of the separately-excited dc motor speed $n$ as a function of the armature voltage $E_A$ to demonstrate that the motor speed is proportional to the armature voltage under no-load conditions.

13. In LVDAC-EMS, open the **Data Table** window. Set the **Data Table** to record the dc motor rotation speed $n$ and torque $T$ (indicated by the **Speed** and **Torque** meters in the **Four-Quadrant Dynamometer/Power Supply** window), as well as the dc motor armature voltage $E_A$, armature current $I_A$, and field current $I_F$ (indicated by meters $E1$, $I1$, and $I2$ in the **Metering** window).

14. In the **Four-Quadrant Dynamometer/Power Supply** window, set the **Torque** parameter to 0.0 N·m (or 0.0 lbf·in).

15. Turn the **Power Supply** on by setting the main power switch to the I (on) position.

   On the **DC Motor/Generator**, set the **Field Rheostat** knob so that the field current $I_F$ (indicated by meter $I2$ in the **Metering** window) is equal to the value indicated in Table 2-1 for your local ac power network.
16. On the **Power Supply**, vary the voltage control knob setting from 0% to 100% in 10% steps in order to increase the armature voltage $E_a$ by steps. For each setting, wait until the motor speed stabilizes, then record the motor armature voltage $E_a$, armature current $I_a$, and field current $I_f$, as well as the motor rotation speed $n$ and torque $T$ in the **Data Table**.

17. When all data has been recorded, stop the **DC Motor/Generator** by setting the voltage control knob to 0% and the main power switch of the **Power Supply** to the O (off) position. (Leave the 24 V ac power source of the **Power Supply** turned on.)

In the **Data Table** window, confirm that the data has been stored, save the data table under filename DT211, and print the data table if desired.

The results obtained are presented below.

**Armature voltage, armature current, field current, rotation speed, and torque of the separately-excited dc motor (DT211).**

<table>
<thead>
<tr>
<th>Motor armature voltage $E_a$ (V)</th>
<th>Motor armature current $I_a$ (A)</th>
<th>Motor field current $I_f$ (A)</th>
<th>Motor speed $n$ (r/min)</th>
<th>Motor torque $T$ (N·m or lbf·in)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.00</td>
<td>0.00</td>
<td>0.300</td>
<td>0</td>
<td>0.00 N·m (0.00 lbf·in)</td>
</tr>
<tr>
<td>14.15</td>
<td>0.443</td>
<td>0.300</td>
<td>146</td>
<td>0.20 N·m (1.77 lbf·in)</td>
</tr>
<tr>
<td>27.71</td>
<td>0.512</td>
<td>0.299</td>
<td>326</td>
<td>0.22 N·m (1.95 lbf·in)</td>
</tr>
<tr>
<td>41.66</td>
<td>0.550</td>
<td>0.298</td>
<td>511</td>
<td>0.25 N·m (2.21 lbf·in)</td>
</tr>
<tr>
<td>55.49</td>
<td>0.592</td>
<td>0.298</td>
<td>694</td>
<td>0.28 N·m (2.48 lbf·in)</td>
</tr>
<tr>
<td>68.55</td>
<td>0.609</td>
<td>0.297</td>
<td>866</td>
<td>0.30 N·m (2.48 lbf·in)</td>
</tr>
</tbody>
</table>
### Motor armature voltage $E_A$ (V) | Motor armature current $I_A$ (A) | Motor field current $I_f$ (A) | Motor speed $n$ (r/min) | Motor torque $T$ (N·m or lbf·in)
--- | --- | --- | --- | ---
82.27 | 0.640 | 0.297 | 1051 | 0.31 N·m (2.66 lbf·in)
96.17 | 0.651 | 0.297 | 1232 | 0.31 N·m (2.74 lbf·in)
109.7 | 0.678 | 0.296 | 1406 | 0.32 N·m (2.83 lbf·in)
124.4 | 0.686 | 0.296 | 1592 | 0.33 N·m (2.92 lbf·in)
138.3 | 0.695 | 0.297 | 1764 | 0.35 N·m (3.10 lbf·in)

18. In the Graph window, make the appropriate settings to obtain a graph of the dc motor speed $n$ as a function of the armature voltage $E_A$. Name the graph "G211", name the x-axis "Armature voltage", name the y-axis "Motor speed", and print the graph if desired.

The resulting graph is shown below.

Separately-excited dc motor speed $n$ versus armature voltage $E_A$ (G211).

What kind of relationship exists between the armature voltage $E_A$ and dc motor speed $n$?

A linear relationship (see figure above)
Does this graph confirm that the separately-excited dc motor is equivalent to a linear voltage-to-speed converter, with higher voltage producing greater speed?

☐ Yes  ☐ No

Yes

19. Use the two end points to calculate the slope $K_1$ of the relationship obtained in graph G211. The values of these points are indicated in data table DT211.

$$K_1 = \frac{n_2 - n_1}{E_2 - E_1} = \frac{-1764 \text{ r/min} - 0 \text{ r/min}}{138 \text{ V} - 0 \text{ V}} = 12.9 \text{ r/min/V}$$

20. In the Data Table window, clear the recorded data.

Motor torque versus armature current

In this section, you will measure data and plot a graph of the separately-excited dc motor torque $T$ as a function of the armature current $I_A$ to demonstrate that the motor torque is proportional to the armature current.

21. In the Four-Quadrant Dynamometer/Power Supply window, make sure that the Torque parameter is set to 0.0 N·m (0.0 lbf·in).

22. Turn the Power Supply on by setting the main power switch to the I (on) position.

On the DC Motor/Generator, slightly readjust the Field Rheostat knob, if necessary, so that the field current $I_f$ (indicated by meter $I_2$ in the Metering window) is equal to the value indicated in Table 2-1 for your local ac power network.

On the Power Supply, set the voltage control knob so that the motor rotation speed $n$ is 1500 r/min. Note and record the value of the motor armature voltage $E_A (E1)$.

Armature voltage $E_A (n = 1500 \text{ r/min}) = _____ \text{ V}$

Motor armature voltage $E_A (n = 1500 \text{ r/min}) = 117 \text{ V}$
Note and record the value of the motor torque \( T \) indicated by the Torque meter in the Four-Quadrant Dynamometer/Power Supply.

Motor torque \( T \) (minimum) = _______ N\cdot m (lbf\cdot in)

Motor torque \( T \) (minimum) = 0.33 N\cdot m (2.9 lbf\cdot in)

23. In the Four-Quadrant Dynamometer/Power Supply window, set the Torque parameter to the minimum value measured in step 22. Record the motor rotation speed \( n \) and torque \( T \), as well as the motor armature voltage \( E_a \), armature current \( I_A \), and field current \( I_F \) in the Data Table.

Increase the Torque parameter from the minimum value to about 1.9 N\cdot m (about 16.8 lbf\cdot in) if your local ac power network voltage is 120 V, or from the minimum value to about 2.3 N\cdot m (about 20.4 lbf\cdot in) if your local ac power network voltage is 220 V or 240 V, in steps of 0.2 N\cdot m (or 2.0 lbf\cdot in). For each torque setting, readjust the voltage control knob of the Power Supply so that the armature voltage \( E_a \) remains equal to the value recorded in step 22, readjust the field current \( I_F \) to the value given in Table 2-1, then record the motor rotation speed \( n \) and torque \( T \), as well as the motor armature voltage \( E_a \), armature current \( I_A \), and field current \( I_F \) in the Data Table.

**CAUTION**

The armature current \( I_A \) will exceed the rated value while performing this manipulation. Therefore, perform this manipulation in less than 5 minutes.

24. When all data has been recorded, stop the DC Motor/Generator by setting the voltage control knob to 0% and the main power switch of the Power Supply to the O (off) position. (Leave the 24 V ac power source of the Power Supply turned on).

In the Four-Quadrant Dynamometer/Power Supply window, set the Torque parameter to 0.0 N\cdot m (0.0 lbf\cdot in).

In the Data Table window, confirm that the data has been stored, save the data table under filename DT212, and print the data table if desired.
The results obtained are presented below.

When the motor torque $T$ is expressed in N·m:

Armature voltage, armature current, field current, rotation speed, and torque (expressed in N·m) of the separately-excited dc motor (DT212).

<table>
<thead>
<tr>
<th>Motor armature voltage $E_A$ (V)</th>
<th>Motor armature current $I_A$ (A)</th>
<th>Motor field current $I_f$ (A)</th>
<th>Motor rotation speed $n$ (r/min)</th>
<th>Motor torque $T$ (N·m)</th>
</tr>
</thead>
<tbody>
<tr>
<td>117</td>
<td>0.654</td>
<td>0.300</td>
<td>1500</td>
<td>0.33</td>
</tr>
<tr>
<td>117</td>
<td>0.960</td>
<td>0.300</td>
<td>1461</td>
<td>0.53</td>
</tr>
<tr>
<td>117</td>
<td>1.275</td>
<td>0.300</td>
<td>1424</td>
<td>0.74</td>
</tr>
<tr>
<td>117</td>
<td>1.583</td>
<td>0.300</td>
<td>1395</td>
<td>0.93</td>
</tr>
<tr>
<td>117</td>
<td>1.891</td>
<td>0.300</td>
<td>1367</td>
<td>1.14</td>
</tr>
<tr>
<td>117</td>
<td>2.212</td>
<td>0.301</td>
<td>1333</td>
<td>1.34</td>
</tr>
<tr>
<td>117</td>
<td>2.550</td>
<td>0.300</td>
<td>1308</td>
<td>1.53</td>
</tr>
<tr>
<td>117</td>
<td>2.895</td>
<td>0.300</td>
<td>1278</td>
<td>1.74</td>
</tr>
<tr>
<td>117</td>
<td>3.261</td>
<td>0.300</td>
<td>1246</td>
<td>1.93</td>
</tr>
</tbody>
</table>

When the motor torque $T$ is expressed in lbf·in:

Armature voltage, armature current, field current, rotation speed, and torque (expressed in lbf·in) of the separately-excited dc motor (DT212).

<table>
<thead>
<tr>
<th>Motor armature voltage $E_A$ (V)</th>
<th>Motor armature current $I_A$ (A)</th>
<th>Motor field current $I_f$ (A)</th>
<th>Motor rotation speed $n$ (r/min)</th>
<th>Motor torque $T$ (lbf·in)</th>
</tr>
</thead>
<tbody>
<tr>
<td>117</td>
<td>0.619</td>
<td>0.300</td>
<td>1500</td>
<td>2.93</td>
</tr>
<tr>
<td>117</td>
<td>0.958</td>
<td>0.300</td>
<td>1460</td>
<td>4.94</td>
</tr>
<tr>
<td>117</td>
<td>1.285</td>
<td>0.300</td>
<td>1417</td>
<td>6.95</td>
</tr>
<tr>
<td>117</td>
<td>1.625</td>
<td>0.300</td>
<td>1378</td>
<td>8.94</td>
</tr>
<tr>
<td>117</td>
<td>1.993</td>
<td>0.300</td>
<td>1347</td>
<td>10.9</td>
</tr>
<tr>
<td>117</td>
<td>2.363</td>
<td>0.300</td>
<td>1314</td>
<td>12.9</td>
</tr>
<tr>
<td>117</td>
<td>2.761</td>
<td>0.300</td>
<td>1283</td>
<td>14.9</td>
</tr>
<tr>
<td>117</td>
<td>3.188</td>
<td>0.300</td>
<td>1249</td>
<td>16.9</td>
</tr>
</tbody>
</table>

25. In the Graph window, make the appropriate settings to obtain a graph of the dc motor torque $T$ as a function of the armature current $I_A$. Name the graph “G212”, name the x-axis “Armature current”, name the y-axis “Motor torque”, and print the graph if desired.
The resulting graphs are shown below.

When the motor torque $T$ is expressed in N·m:

Separately-excited dc motor torque $T$ (expressed in N·m) versus armature current $I_a$ (G212).

When the motor torque $T$ is expressed in lbf·in:

Separately-excited dc motor torque $T$ (expressed in lbf·in) versus armature current $I_a$ (G212).
What kind of relationship exists between the armature current $I_A$ and the dc motor torque $T$ as long as the armature current does not exceed the nominal value?

A linear relationship (see figure)

Does this graph confirm that the separately-excited dc motor is equivalent to a linear current-to-torque converter (when the armature current does not exceed the nominal value), with higher current producing greater torque?

☐ Yes  ☐ No

*The torque-versus-current relationship is no longer linear when the armature current $I_A$ exceeds the nominal value because of a phenomenon called armature reaction. This phenomenon is described in the next unit of this manual.*

Yes

26. Use the two end points of the linear portion of the relationship obtained in graph G212 to calculate the slope $K_2$. The values of these points are indicated in data table DT212.

$$K_2 = \frac{T_2 - T_1}{I_2 - I_1} = \frac{N \cdot m}{A}$$

When the motor torque $T$ is expressed in N·m:

$$K_2 = \frac{T_2 - T_1}{I_2 - I_1} = \frac{1.74 \text{ N} \cdot \text{m} - 0.33 \text{ N} \cdot \text{m}}{2.90 \text{ A} - 0.65 \text{ A}} = \frac{0.63 \text{ N} \cdot \text{m}}{A}$$

When the motor torque $T$ is expressed in lbf·in:

$$K_2 = \frac{T_2 - T_1}{I_2 - I_1} = \frac{14.9 \text{ lbf} \cdot \text{in} - 2.93 \text{ lbf} \cdot \text{in}}{2.76 \text{ A} - 0.62 \text{ A}} = \frac{5.59 \text{ lbf} \cdot \text{in}}{A}$$
**Speed decrease versus armature current**

*In this section, you will demonstrate that when the armature voltage $E_A$ is set to a fixed value, the speed of the separately-excited dc motor decreases with increasing armature current or torque because of the increasing voltage drop across the armature resistor.*

**27.** Using the values determined previously for the armature resistance $R_A$ (step 11), constant $K_1$ (step 19), and armature voltage $E_A$ (step 22), calculate the motor rotation speed $n$ for each of the three armature currents $I_A$ given in Table 2-2 for your local ac power network.

$$E_{RA} = I_A \times R_A$$

$$E_{CEMF} = E_A - E_{RA}$$

$$n = E_{CEMF} \times K_1$$

**Table 2-2. DC motor armature currents $I_A$.**

<table>
<thead>
<tr>
<th>Local ac power network</th>
<th>Armature current $I_A$ (A)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voltage (V)</td>
<td>Frequency (Hz)</td>
</tr>
<tr>
<td>120</td>
<td>60</td>
</tr>
<tr>
<td>220</td>
<td>50</td>
</tr>
<tr>
<td>240</td>
<td>50</td>
</tr>
<tr>
<td>220</td>
<td>60</td>
</tr>
</tbody>
</table>

When $I_A = _____$ A:

$E_{RA} = _____$ V

$E_{CEMF} = _____$ V

$n = _____$ r/min

When $I_A = 1.0$ A:

$E_{RA} = 7.6$ V

$E_{CEMF} = 109.4$ V

$n = 1411$ r/min
When $I_A = \_\_\_\_ \text{ A}$:

$E_{RA} = \_\_\_\_ \text{ V}$

$E_{CEMF} = \_\_\_\_ \text{ V}$

$n = \_\_\_\_ \text{ r/min}$

__________________________

When $I_A = 2.0 \text{ A}$:

$E_{RA} = 15.2 \text{ V}$

$E_{CEMF} = 101.8 \text{ V}$

$n = 1313 \text{ r/min}$

__________________________

When $I_A = \_\_\_\_ \text{ A}$:

$E_{RA} = \_\_\_\_ \text{ V}$

$E_{CEMF} = \_\_\_\_ \text{ V}$

$n = \_\_\_\_ \text{ r/min}$

__________________________

When $I_A = 3.0 \text{ A}$:

$E_{RA} = 22.8 \text{ V}$

$E_{CEMF} = 94.2 \text{ V}$

$n = 1215 \text{ r/min}$

__________________________

Based on your results, how should voltage $E_{CEMF}$ and the dc motor speed $n$ vary as the armature current $I_A$ is increased?

The dc motor voltage $E_{CEMF}$ and speed $n$ should decrease when the armature current $I_A$ is increased.

28. In the Graph window, make the appropriate settings to obtain a graph of the dc motor speed $n$ as a function of the armature current $I_A$, using the data recorded previously in data table DT212. Name the graph “G212-1”, name the x-axis “Armature current”, name the y-axis “Motor speed”, and print the graph if desired.
The resulting graph is shown below.

Separately-excited dc motor speed \( n \) versus armature current \( I_A \) (G212-1).

Does graph G212-1 confirm the prediction you made in the previous step about the variation of the dc motor speed \( n \) as a function of the armature current \( I_A \)?

- Yes  - No

Yes (see figure above).

Briefly explain what causes the dc motor speed \( n \) to decrease when the armature voltage \( E_A \) is fixed and the armature current \( I_A \) increases.

The decrease in motor speed \( n \) is caused by the increasing voltage drop across the armature resistor as the armature current \( I_A \) increases.

29. In the Graph window, make the appropriate settings to obtain a graph of the dc motor speed \( n \) as a function of the dc motor torque \( T \) using the data recorded previously in data table DT212. Name the graph “G212-2”, name the x-axis “Motor torque”, name the y-axis “Motor speed”, and print the graph. This graph will be used in the next exercise of this unit.
The resulting graphs are shown below.

When the motor torque $T$ is expressed in N·m:

Separately-excited dc motor speed $n$ versus motor torque $T$ (G212-2).

When the motor torque $T$ is expressed in lbf·in:

Separately-excited dc motor speed $n$ versus motor torque $T$ (G212-2).

If you want to perform the additional experiments, skip the next step, then return to it when all additional manipulations are finished.
30. On the Power Supply, make sure that the main power switch is set to the O (off) position, then turn the 24 V ac power source off. Close the LVDAC-EMS software. Turn the Four-Quadrant Dynamometer/Power Supply off. Disconnect all leads and return them to their storage location.

Additional experiments (optional)

Motor speed-versus-armature voltage and motor torque-versus-armature current characteristics for reversed armature connections

You can obtain graphs of the dc motor speed \( \eta \) as a function of the armature voltage \( E_a \), and dc motor torque \( T \) as a function of the armature current \( I_A \), with reversed armature connections. To do so, make sure that the Power Supply is turned off [main power switch set to the O (off) position] and reverse the connections at the variable dc voltage output (voltage source \( E_s \)) in Figure 2-16. Make sure that the voltage control knob of the Power Supply is set to 0%. Refer to steps 13 to 25 of this exercise to record the necessary data and obtain the graphs. This will allow you to verify that the linear relationships between the motor speed \( \eta \) and armature voltage \( E_A \), and between the motor torque \( T \) and armature current \( I_A \), are valid regardless of the polarity of the armature voltage \( E_A \). Recalculating constants \( K_1 \) and \( K_2 \) will show you that their values are independent of the armature voltage polarity.

Motor speed-versus-armature voltage characteristic for reversed armature connections

Armature voltage, armature current, field current, rotation speed, and torque of the separately-excited dc motor (for reversed armature connections).

<table>
<thead>
<tr>
<th>Motor armature voltage ( E_A ) (V)</th>
<th>Motor armature current ( I_A ) (A)</th>
<th>Motor field current ( I_f ) (A)</th>
<th>Motor rotation speed ( \eta ) (r/min)</th>
<th>Motor torque ( T ) (N·m or lbf·in)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.037</td>
<td>0.00</td>
<td>0.300</td>
<td>0</td>
<td>0.00 N·m (0.00 lbf·in)</td>
</tr>
<tr>
<td>-13.47</td>
<td>-0.444</td>
<td>0.300</td>
<td>-136</td>
<td>-0.19 N·m (-1.68 lbf·in)</td>
</tr>
<tr>
<td>-27.63</td>
<td>-0.492</td>
<td>0.300</td>
<td>-326</td>
<td>-0.22 N·m (-1.95 lbf·in)</td>
</tr>
<tr>
<td>-40.94</td>
<td>-0.521</td>
<td>0.298</td>
<td>-506</td>
<td>-0.24 N·m (-2.12 lbf·in)</td>
</tr>
<tr>
<td>-54.51</td>
<td>-0.542</td>
<td>0.298</td>
<td>-690</td>
<td>-0.26 N·m (-2.30 lbf·in)</td>
</tr>
<tr>
<td>-68.3</td>
<td>-0.556</td>
<td>0.297</td>
<td>-877</td>
<td>-0.28 N·m (-2.48 lbf·in)</td>
</tr>
<tr>
<td>-82.07</td>
<td>-0.581</td>
<td>0.297</td>
<td>-1061</td>
<td>-0.29 N·m (-2.57 lbf·in)</td>
</tr>
</tbody>
</table>
### Ex. 2-1 – The Separately-Excited DC Motor

#### Procedure

Separately-excited dc motor speed $\omega$ versus armature voltage $E_A$ (for reversed armature connections).

<table>
<thead>
<tr>
<th>Motor armature voltage $E_A$ (V)</th>
<th>Motor armature current $I_A$ (A)</th>
<th>Motor field current $I_f$ (A)</th>
<th>Motor rotation speed $\omega$ (r/min)</th>
<th>Motor torque $T$ (N·m or lbf·in)</th>
</tr>
</thead>
<tbody>
<tr>
<td>-96.33</td>
<td>-0.592</td>
<td>0.297</td>
<td>-1255</td>
<td>-0.30 N·m (-2.66 lbf·in)</td>
</tr>
<tr>
<td>-110.1</td>
<td>-0.604</td>
<td>0.297</td>
<td>-1439</td>
<td>-0.32 N·m (-2.83 lbf·in)</td>
</tr>
<tr>
<td>-124.9</td>
<td>-0.62</td>
<td>0.297</td>
<td>-1630</td>
<td>-0.33 N·m (-2.92 lbf·in)</td>
</tr>
<tr>
<td>-138.4</td>
<td>-0.635</td>
<td>0.297</td>
<td>-1813</td>
<td>-0.35 N·m (-3.09 lbf·in)</td>
</tr>
</tbody>
</table>

![Graph showing separately-excited dc motor speed versus armature voltage](image-url)
Motor torque-versus-armature current characteristic for reversed armature connections

When the motor torque $T$ is expressed in N·m:

Armature voltage, armature current, field current, rotation speed, and torque (expressed in N·m) of the separately-excited dc motor (for reversed armature connections).

<table>
<thead>
<tr>
<th>Motor armature voltage $E_A$ (V)</th>
<th>Motor armature current $I_A$ (A)</th>
<th>Motor field current $I_f$ (A)</th>
<th>Motor rotation speed $n$ (r/min)</th>
<th>Motor torque $T$ (N·m)</th>
</tr>
</thead>
<tbody>
<tr>
<td>-116</td>
<td>-0.570</td>
<td>0.300</td>
<td>-1500</td>
<td>-0.32</td>
</tr>
<tr>
<td>-116</td>
<td>-0.860</td>
<td>0.300</td>
<td>-1461</td>
<td>-0.52</td>
</tr>
<tr>
<td>-116</td>
<td>-1.166</td>
<td>0.300</td>
<td>-1419</td>
<td>-0.72</td>
</tr>
<tr>
<td>-116</td>
<td>-1.463</td>
<td>0.300</td>
<td>-1390</td>
<td>-0.92</td>
</tr>
<tr>
<td>-116</td>
<td>-1.770</td>
<td>0.300</td>
<td>-1360</td>
<td>-1.12</td>
</tr>
<tr>
<td>-116</td>
<td>-2.104</td>
<td>0.300</td>
<td>-1331</td>
<td>-1.32</td>
</tr>
<tr>
<td>-116</td>
<td>-2.429</td>
<td>0.300</td>
<td>-1296</td>
<td>-1.52</td>
</tr>
<tr>
<td>-116</td>
<td>-2.785</td>
<td>0.300</td>
<td>-1268</td>
<td>-1.72</td>
</tr>
<tr>
<td>-116</td>
<td>-3.163</td>
<td>0.300</td>
<td>-1239</td>
<td>-1.92</td>
</tr>
</tbody>
</table>

Separately-excited dc motor torque $T$ (expressed in N·m) versus armature current $I_A$ (for reversed armature connections).
When the motor torque $T$ is expressed in lbf·in:

Armature voltage, armature current, field current, rotation speed, and torque (expressed in lbf·in) of the separately-excited dc motor (for reversed armature connections).

<table>
<thead>
<tr>
<th>Motor armature voltage $E_A$ (V)</th>
<th>Motor armature current $I_A$ (A)</th>
<th>Motor field current $I_F$ (A)</th>
<th>Motor rotation speed $n$ (r/min)</th>
<th>Motor torque $T$ (lbf·in)</th>
</tr>
</thead>
<tbody>
<tr>
<td>-116</td>
<td>-0.564</td>
<td>0.300</td>
<td>-1500</td>
<td>-2.84</td>
</tr>
<tr>
<td>-116</td>
<td>-0.884</td>
<td>0.300</td>
<td>-1455</td>
<td>-4.82</td>
</tr>
<tr>
<td>-116</td>
<td>-1.226</td>
<td>0.300</td>
<td>-1413</td>
<td>-6.82</td>
</tr>
<tr>
<td>-116</td>
<td>-1.561</td>
<td>0.300</td>
<td>-1375</td>
<td>-8.81</td>
</tr>
<tr>
<td>-116</td>
<td>-1.933</td>
<td>0.300</td>
<td>-1338</td>
<td>-10.8</td>
</tr>
<tr>
<td>-116</td>
<td>-2.302</td>
<td>0.300</td>
<td>-1307</td>
<td>-12.8</td>
</tr>
<tr>
<td>-116</td>
<td>-2.675</td>
<td>0.300</td>
<td>-1280</td>
<td>-14.8</td>
</tr>
<tr>
<td>-116</td>
<td>-3.088</td>
<td>0.300</td>
<td>-1245</td>
<td>-16.8</td>
</tr>
</tbody>
</table>

Separately-excited dc motor torque $T$ (expressed in lbf·in) as a function of the armature current $I_A$ (for reversed armature connections).
CONCLUSION

In this exercise, you learned how to measure the armature resistance of a dc motor. You saw that the rotation speed of a separately-excited dc motor is proportional to the armature voltage applied to the motor. You saw that the torque produced by a dc motor is proportional to the armature current. You observed that the dc motor speed decreases with increasing armature current when the armature voltage is fixed. You demonstrated that this speed decrease is caused by the increasing voltage drop across the armature resistor as the armature current increases.

If you performed the additional experiments, you observed that the speed-versus-armature voltage and torque-versus-armature current relationships are not affected by the polarity of the armature voltage. You also observed that the direction of rotation is reversed when the polarity of the armature voltage is reversed.

REVIEW QUESTIONS

1. What kind of relationship exists between the rotation speed and armature voltage of a separately-excited dc motor?
   A linear relationship.

2. What kind of relationship exists between the torque and armature current of a separately-excited dc motor as long as the armature current does not exceed the nominal value?
   A linear relationship.

3. Connecting a dc power source to the armature of a dc motor that operates without field current and measuring the voltage that produces nominal current flow in the armature allows which parameter of the dc motor to be determined?
   The armature resistance.

4. Does the rotation speed of a separately-excited dc motor increase or decrease when the armature current increases?
   The rotation speed decreases.

5. The armature resistance $R_A$ and constant $K_1$ of a dc motor are 0.5 Ω and 5 r/min/V, respectively. A voltage of 200 V is applied to this motor. The no-load armature current is 2 A. At full load, the armature current increases to 50 A. What are the no-load and full-load speeds of the motor?
   The no-load speed is 995 r/min, while the full-load speed is 875 r/min.
Bibliography
